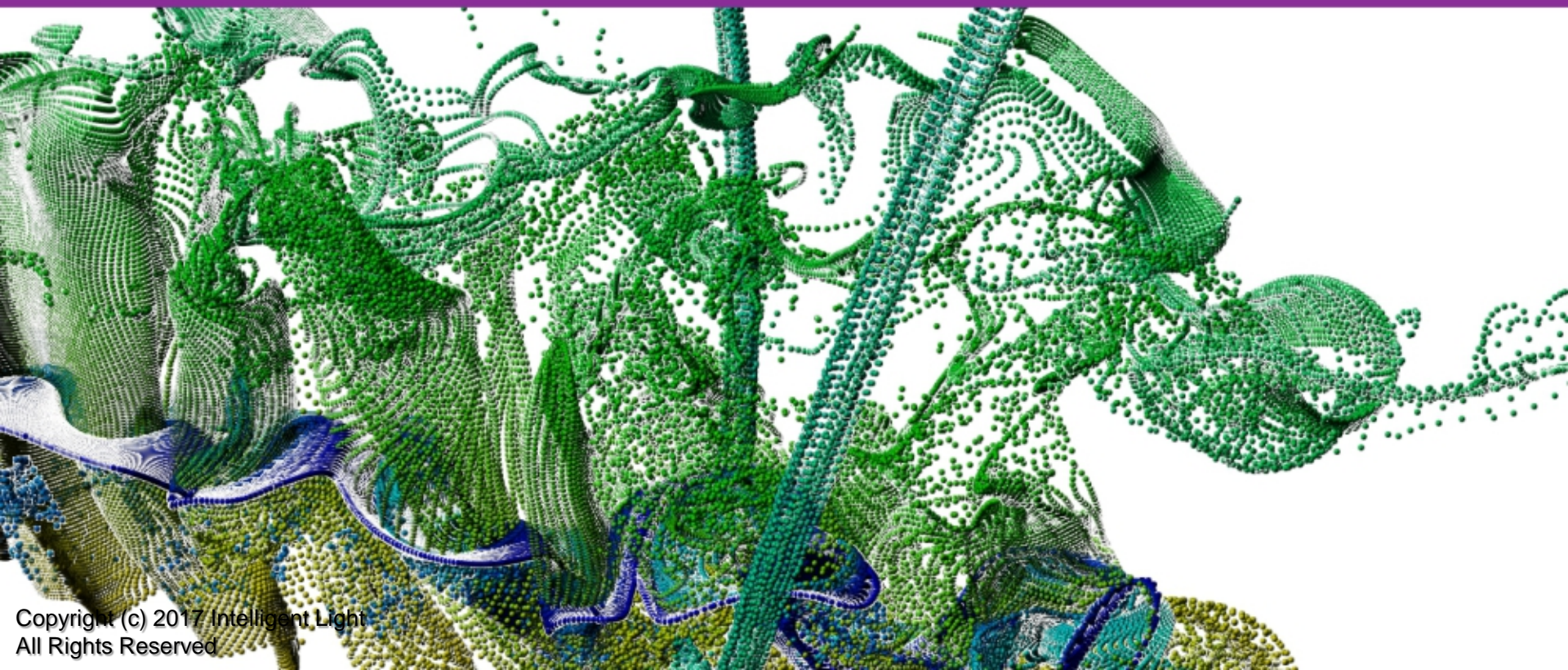


Applied Research Group
Seeking Answers, Deploying Solutions

Intelligent Light



Contribution to HiLiftPW-3

Earl P.N. Duque
Intelligent Light
#040

3rd High Lift Prediction Workshop
Denver, CO June 3-4, 2017

Outline

- Purpose
 - IL's contribution to the knowledge base
 - Exercise UQ methods
- Demonstrate Large scale big data workflow processes with Dakota + FieldView
- Predictive blind study with UQ

AIAA High Lift Prediction Workshop 3

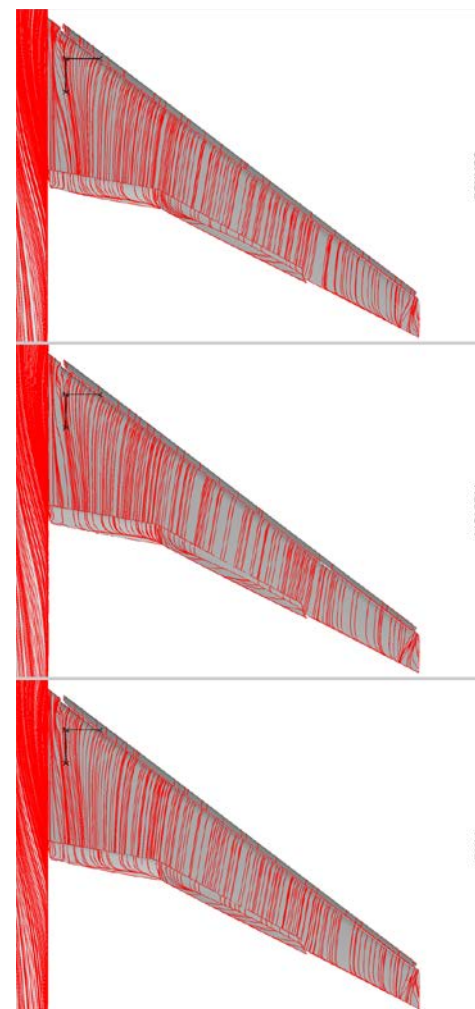
- Case 1a – High Lift CRM Model
 - OVERFLOW2.2I solver
 - Overset Structure #2, Coarse, medium, fine and extra fine grid
 - SA-noft2 Turbulence model
 - Alpha – 8, 16
 - Steady
 - Blind Run up to 50,000 time steps
- Tools Used
 - FieldView – Data extracts for local Diss error
 - VisIt – mesh extracts for local Diss error
 - Dakota – Model input sampling
 - Octave – Global & local UQ calcs, 2-D plots
- Perform UQ
 - Both Global and Local
 - Discretization Uncertainty
 - Model Input Uncertainty Mix Uncertainty
 - Latin Hypercube Sampling
 - Model Input Uncertainty
 - Medium Grid
 - Blind Run 20,000 time steps

Case	Alpha=8, Fully turb, grid study	Alpha=16, Fully turb, grid study	Other
1a (full gap)	yes	yes	OVERFLOW2.2I C,M,F,EF SA-noft2
1b (full gap w adaption)	no	no	
1c (partial seal)	no	no	
1d (partial seal w adaption)	no	no	
Other			

Grid System	Case(s)	If committee grid, report any problems/issues If user grid, reason for generating grid system
Overset Structure #2	1a	Worked very well, no issues
User (Grid type/description)	1a, 2a, 2c...	Generated grid system because...
Other		

OVERFLOW, FieldView, Visit Workflows

- Solver - OVERFLOW-2.2l
 - Cray XE-40
 - Dual socket Broadwell
 - 176-1408 cores Methodologies
 - RHS - Central
 - LHS – Scalar Penta
 - Multi-Grid – 2 levels (FMG = .F.)
 - SA-noft2 Fully Turbulent
- FieldView 16.1
 - Cray XE-40 – 44 cores
 - Automated Batch Post-Processing
 - XDB workflow for surface data extraction and velocity plots
- Visit 2.12.1
 - Local laptop
 - XDB Data extracts for grid volume and skewness

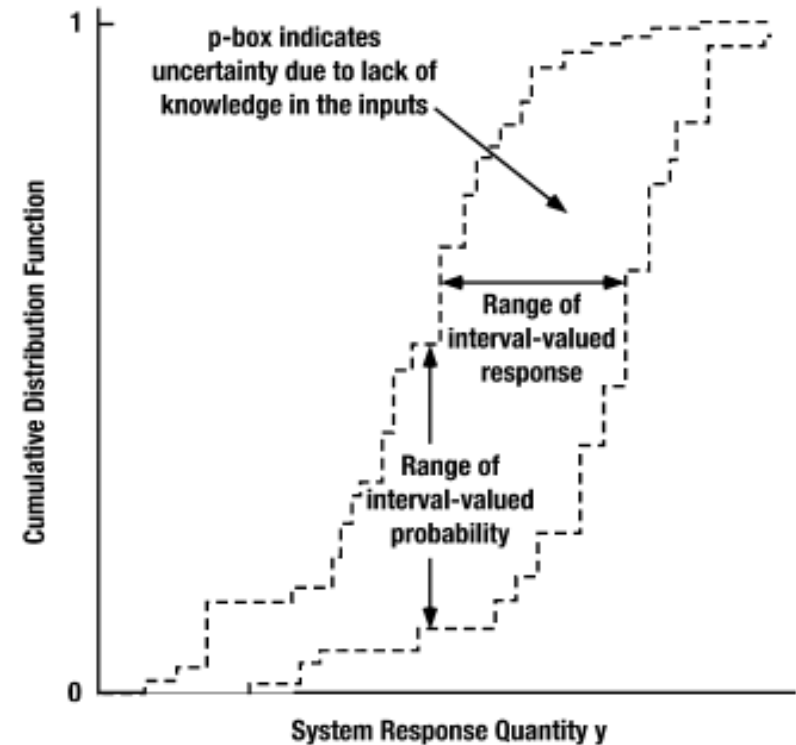




- Dakota from Sandia National Lab has been in existence for two decades.
- Extensive capabilities to perform optimization and UQ studies.
- Well thought out, easy to use, python interface to manage and launch solvers.
- It has considerable capability for sampling, an automated system for launching simulations and various analysis methods.

UQ methodology by Oberkampf and Roy (2010)

- Identify all sources of uncertainty
- Characterize uncertainties
- Propagate input uncertainties through the model
 - Aleatory uncertainty
 - Epistemic uncertainty
 - Combined aleatory and epistemic uncertainty
- Determine total uncertainty in the SRQ
 - $U_{total} = U_{diss} + U_{iter} + U_{Model\ Input} + U_{Model\ Form} + U_{exp}$
 - Results in a P-Box Plot
 - CDF, but with a finite width that denotes the epistemic (lack of knowledge) uncertainty



P-Box plot example

Discretization Error

Celik, et.al. (JFM 2008) & ASME VV20

- Define Representative Grid Size
 - Global – $h_i = N^{2/3}$ (Where i=1- Extrafine, 2-Fine, 3-Medium)
 - Line Plots – $h_i(x, y, z) = V_i(x, y, z)^{1/3}$
 - Refinement ratio - $r_{ij} = h_i/h_j$

- Observed Order – P

$$P = \frac{1}{\ln(r_{21})} \left| \ln \left| \frac{\varepsilon_{32}}{\varepsilon_{21}} \right| + q(p) \right|$$

$$q(p) = \ln \left(\frac{r_{21}^p - s}{r_{32}^p - s} \right) ; s = \text{sig}(\varepsilon_{32}/\varepsilon_{21})$$

Discretization Error

- Calculate Extrapolated Value (Celik, 2008)

$$\phi_{ext}^{21} = (r_{21}^p \phi_1 - \phi_2) / (r_{21}^p - 1)$$

$$\phi_{ext}^{32} = (r_{32}^p \phi_2 - \phi_3) / (r_{32}^p - 1)$$

- Discretization Error

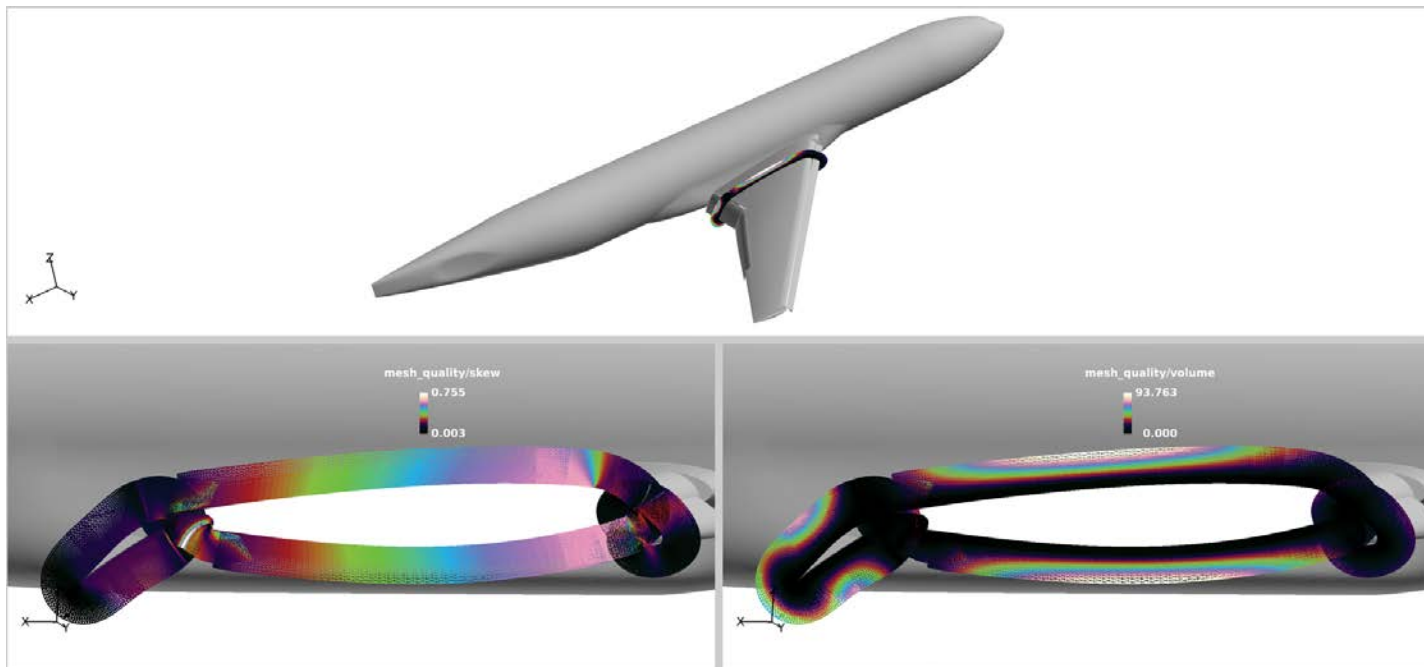
$$U_{num} = \left| \frac{1.25(\phi_1 - \phi_2)}{r_{21}^p - 1} \right|; p > 1 \text{ (Roache, 1998)}$$

$$U_{num} = |3(\phi_3 - \phi_1)|; p < 1 \text{ (Eca, 2009)}$$

- Assume $p = p_{average}$ for local line plots (Celik, 2008)

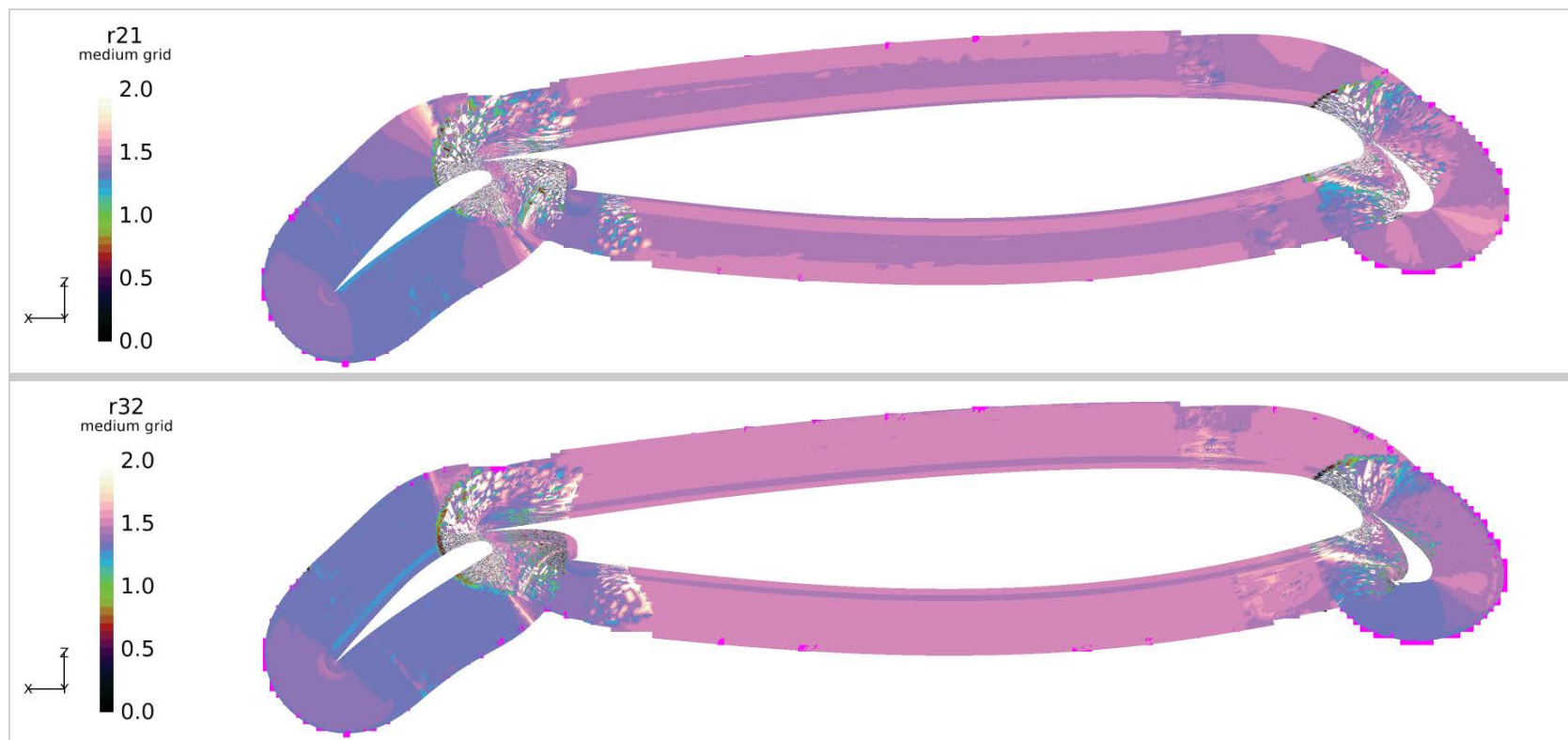
Line plots require Mesh Quality Metrics

- Grid skewness and volume (V) from VisIt to XDB
- XDB used in FieldView to compute the local mesh size and grid refinement levels
- Used medium, fine, extrafine interpolated to medium



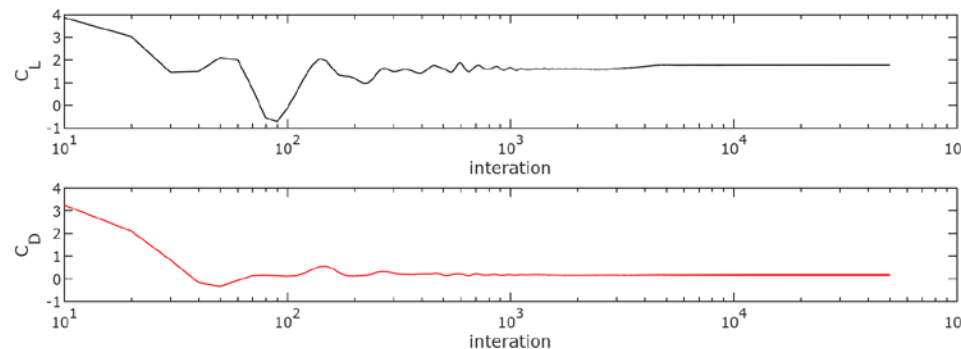
Refinement comparisons

- $h_i(x, y, z) = V_i(x, y, z)^{1/3}$
- 2D cut from the 3D mesh
- $r_{21} = \frac{h_{fine}}{h_{extrafine}}$; $r_{32} = \frac{h_{medium}}{h_{fine}}$
- Mesh is not uniformly refined

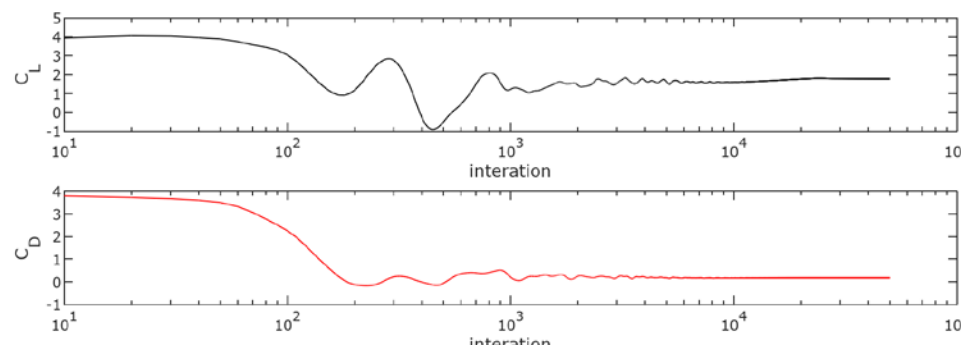


Iteration History – 8 deg

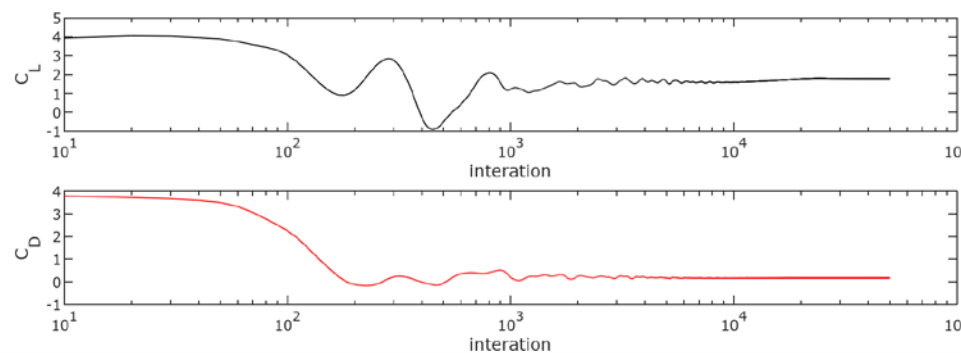
Extrafine



Fine



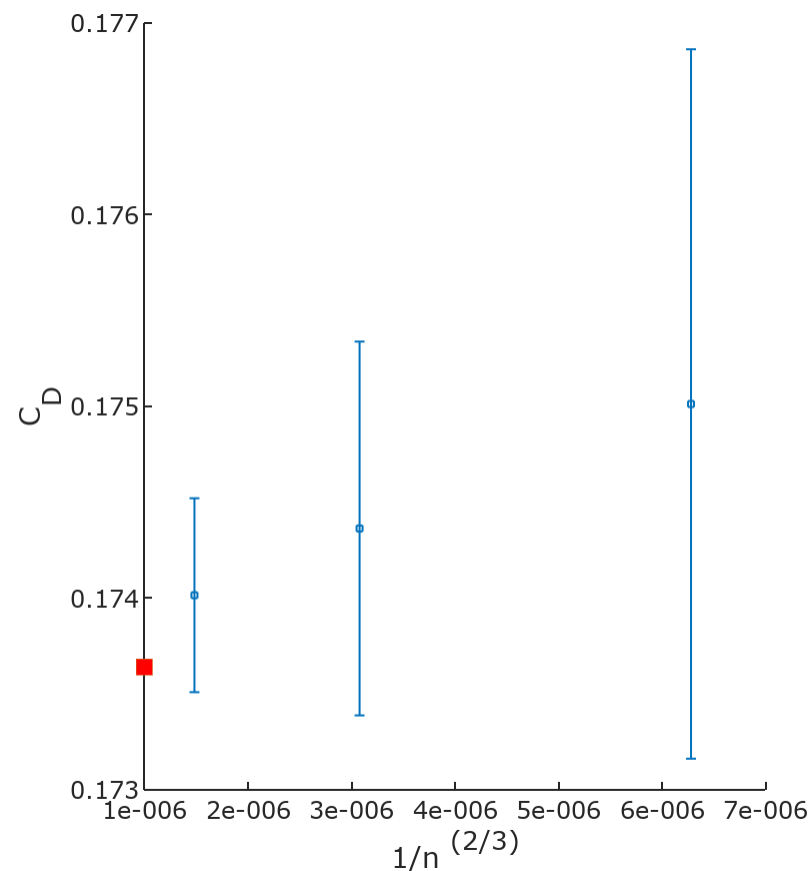
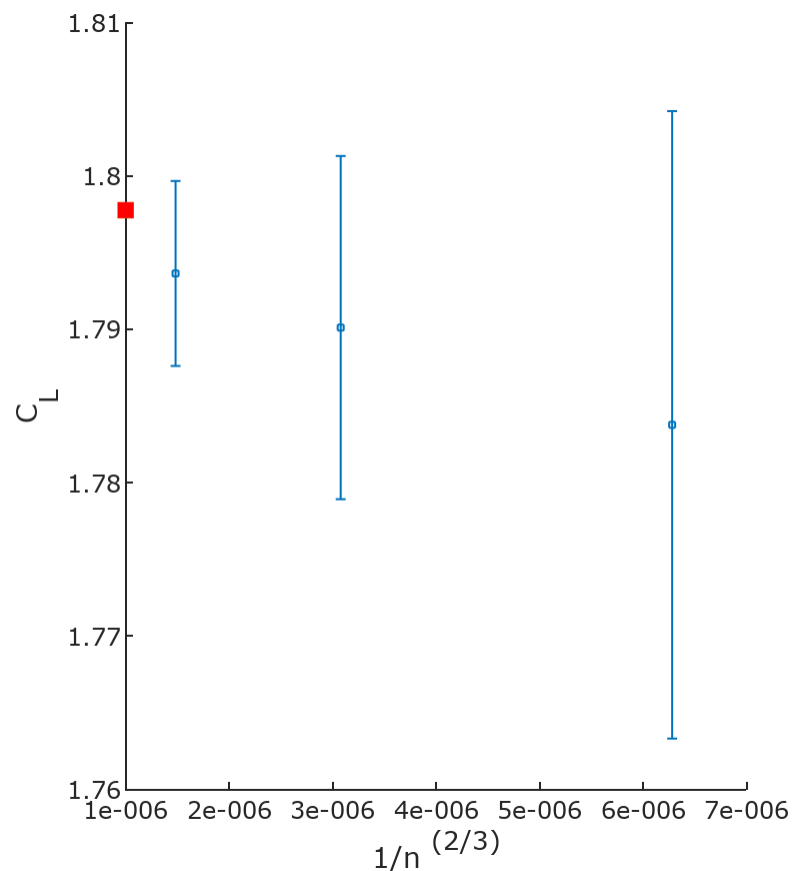
Medium



Discretization Error (DE) – 8 deg

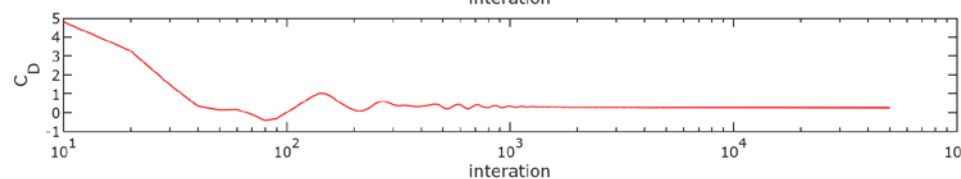
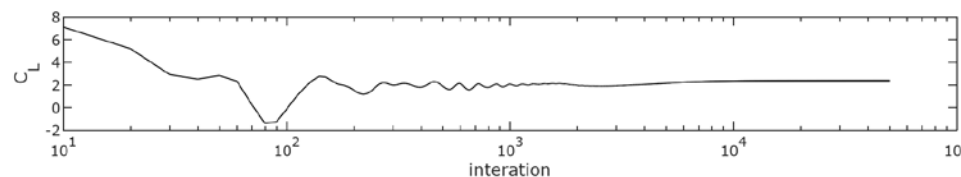
- $P=1.69225$
- $GCI=0.00287513$
- $CI_{exp} = 1.7978$

- $P=1.79687$
- $GCI = 0.00269556$
- $CD_{exp}=0.17364$

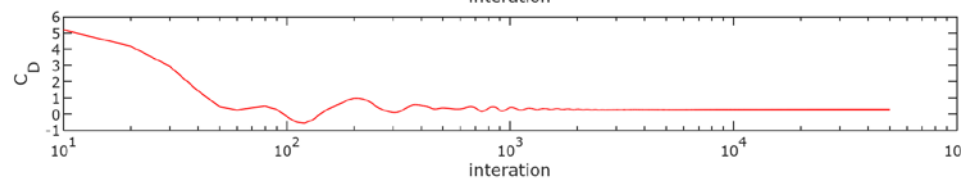
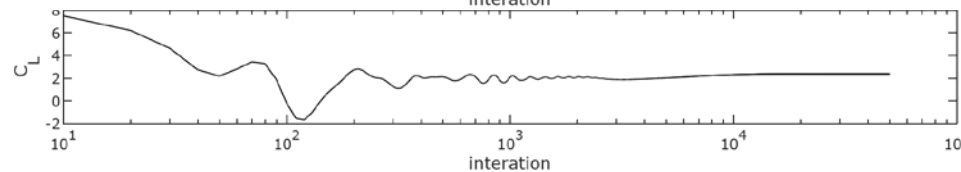


Iteration History – 16 deg

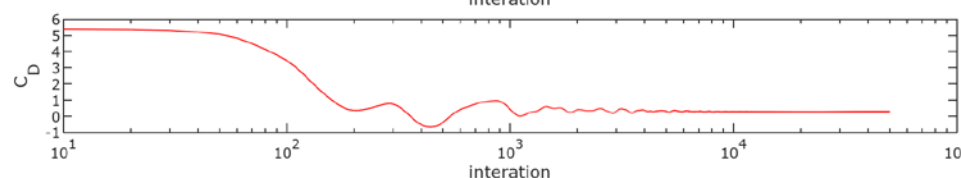
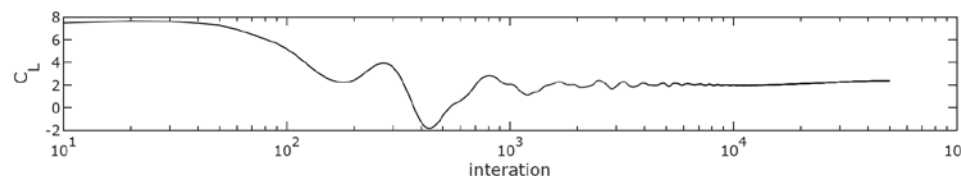
Extrafine



Fine

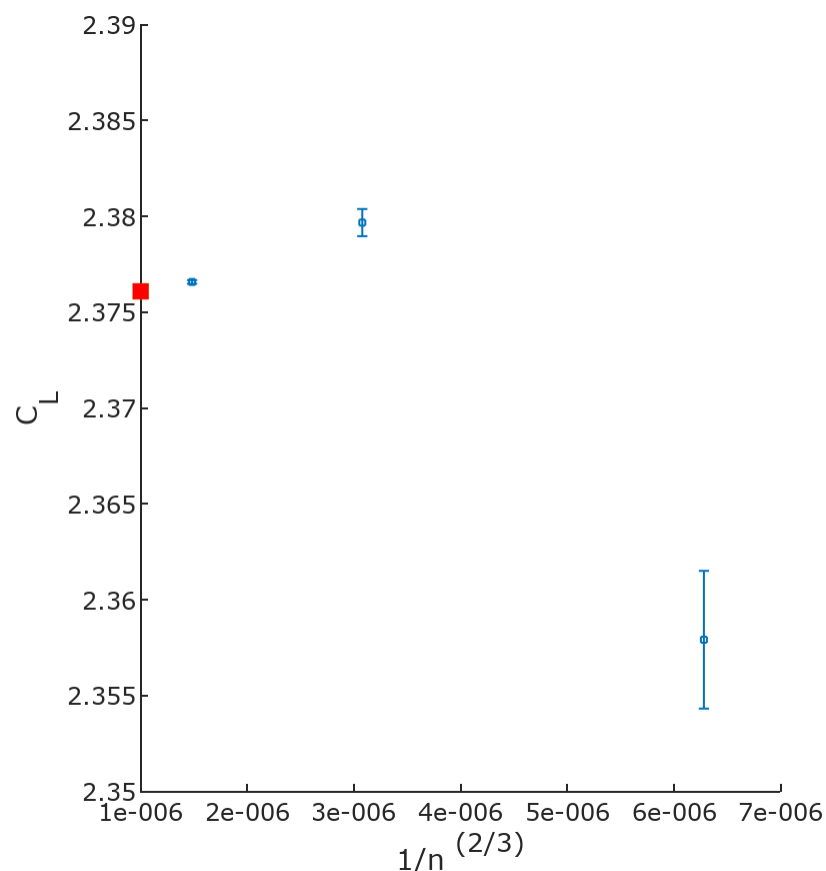


Medium

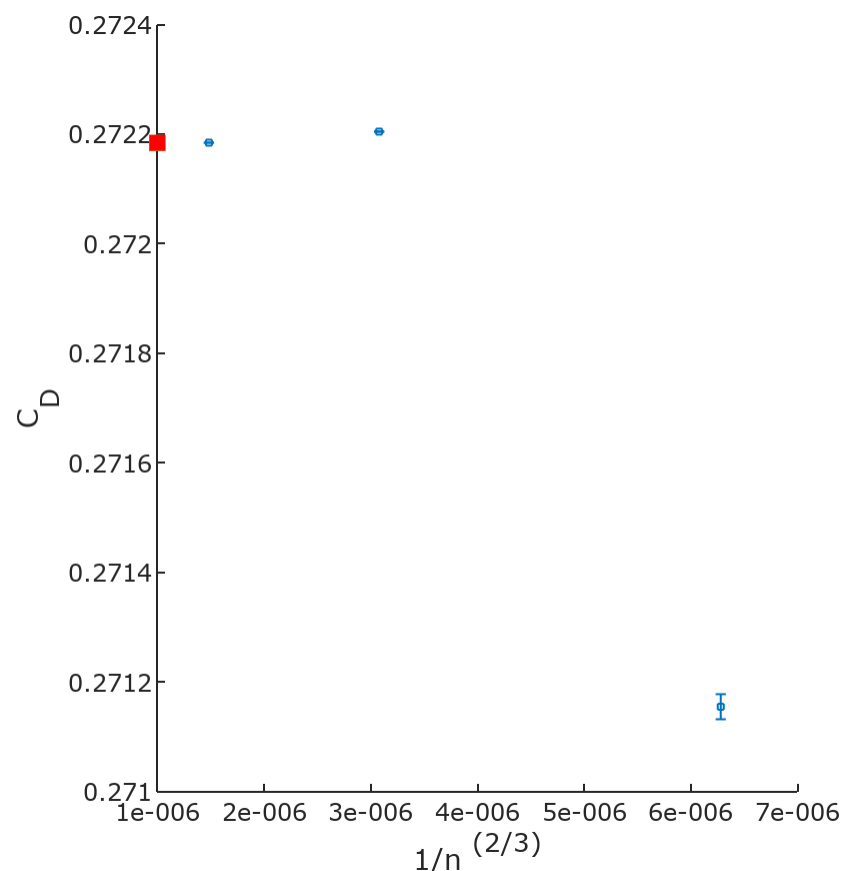


Discretization Error (DE) – 16 deg

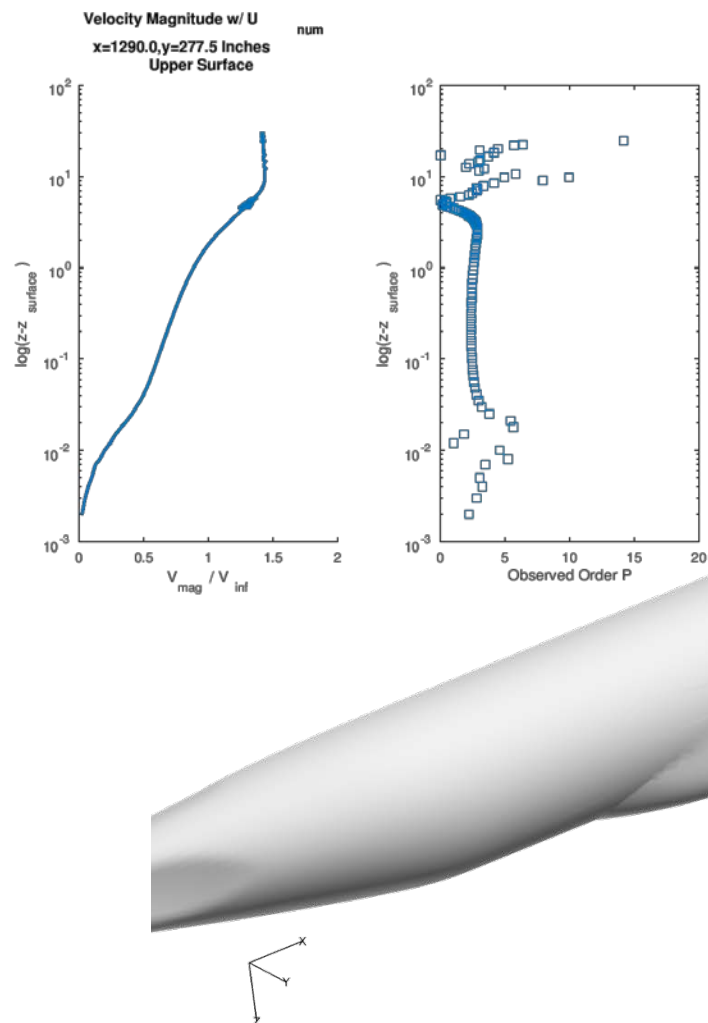
- $P = 5.45217$
- $GCI = 0.000257509$
- $CL_{ext} = 2.376$



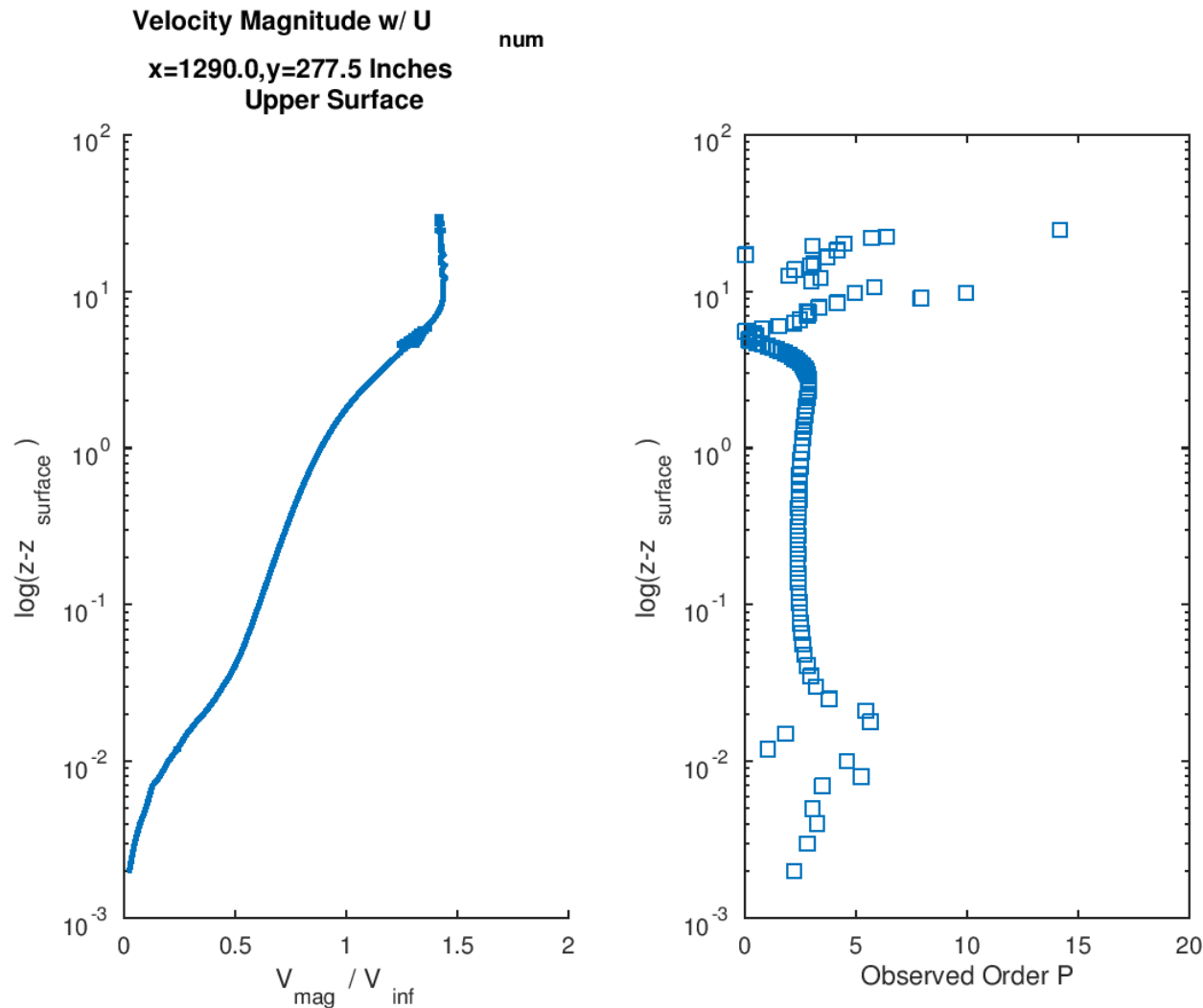
- $P = 11.08$
- $GCI = 1.64845e-006$
- $CD_{ext} = .272$



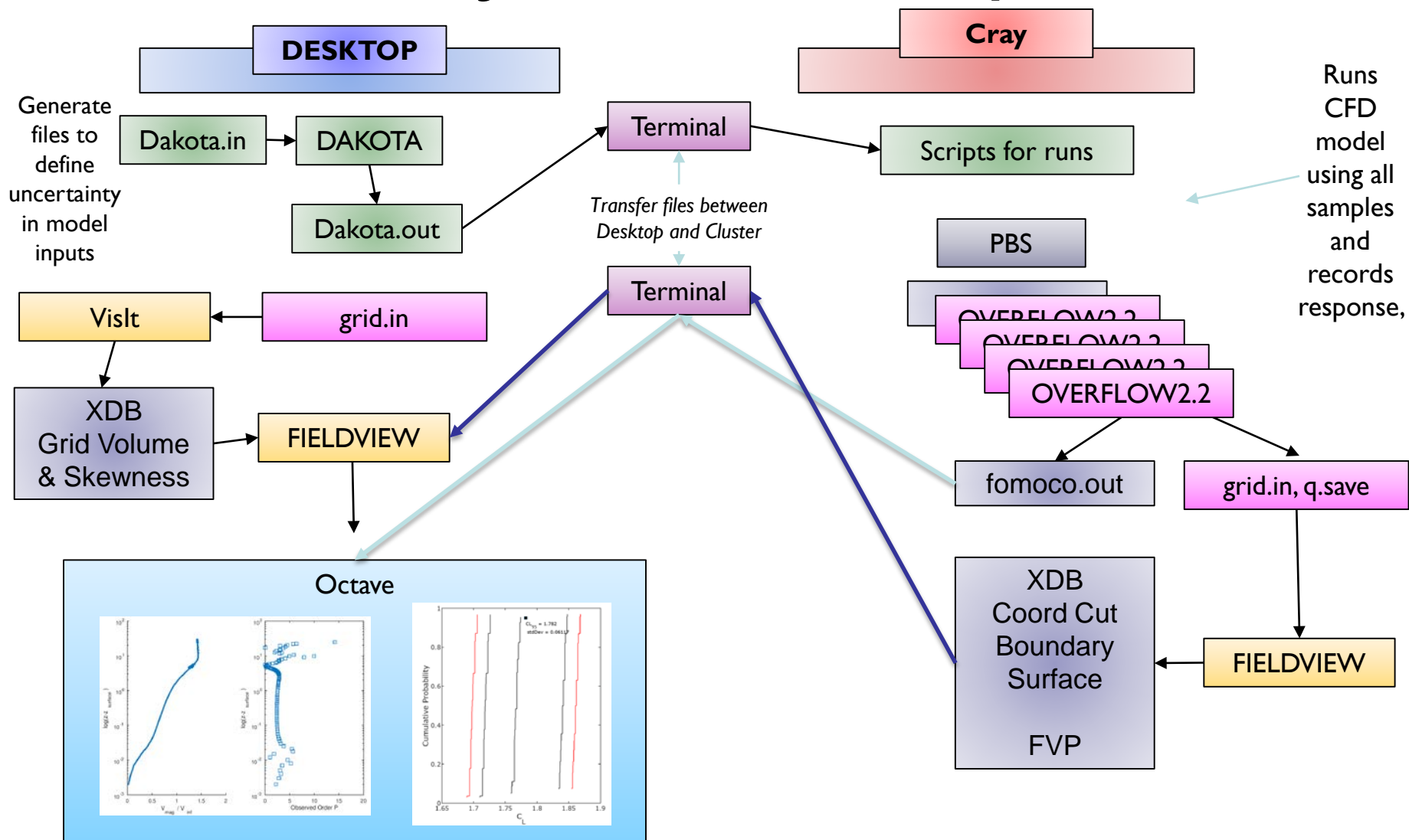
Velocity Plots



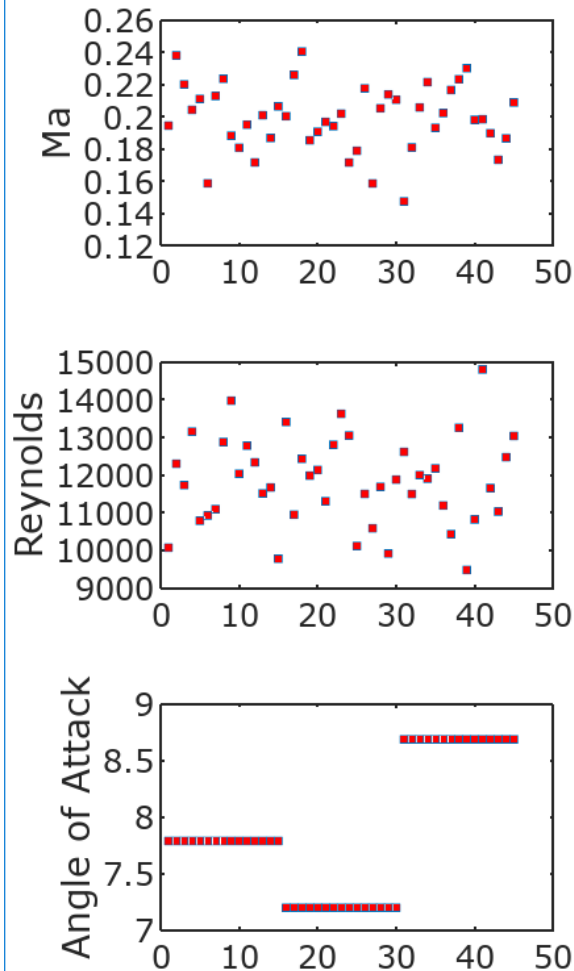
Numerical Uncertainty – 16 Deg



Uncertainty in model inputs



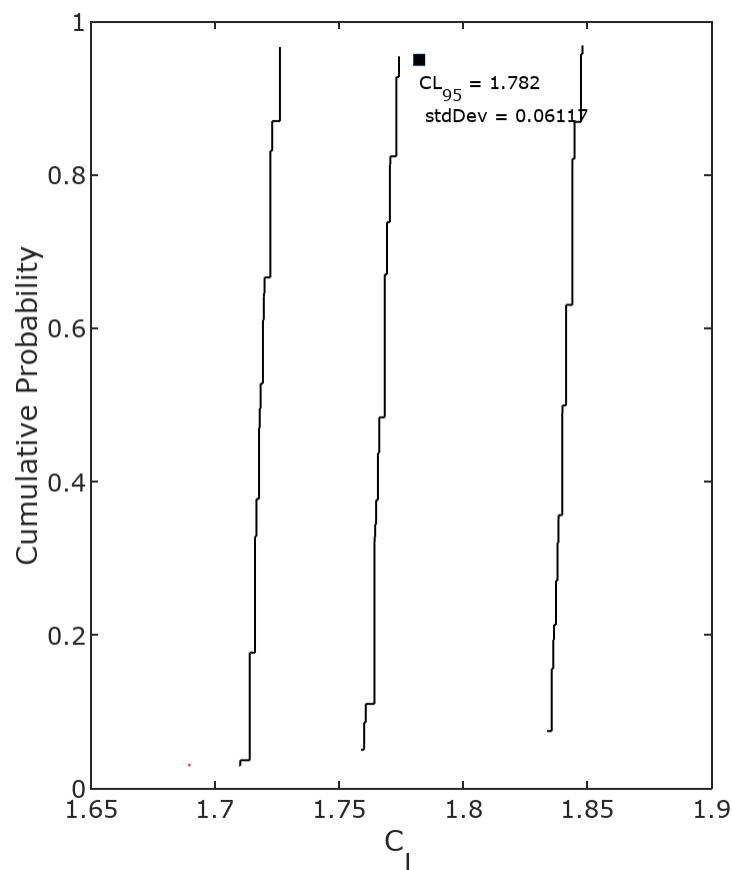
Model Input Uncertainty



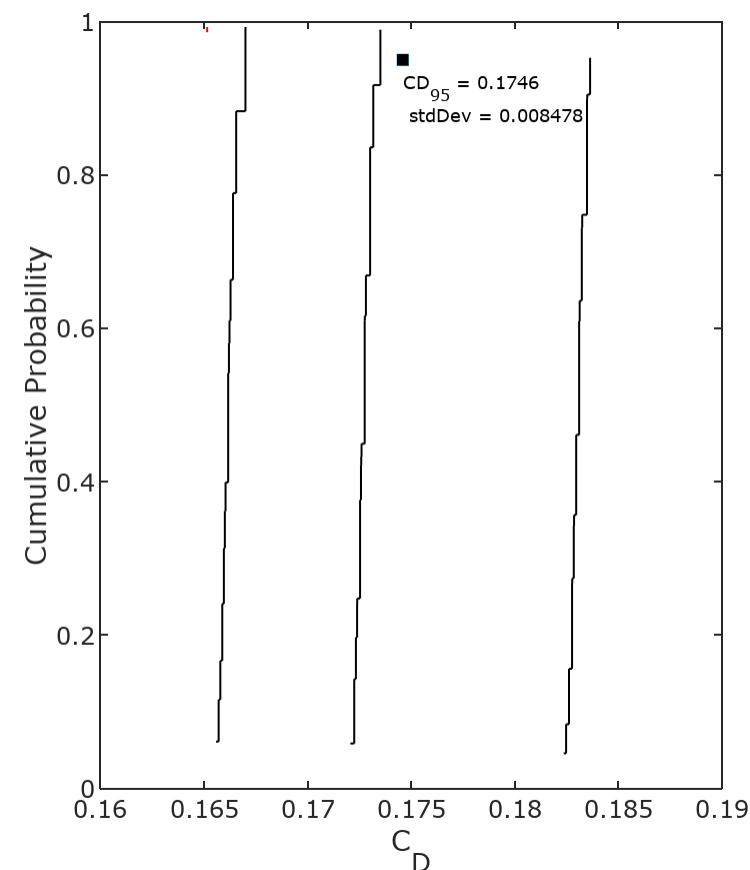
- Aleatory - Gaussian
 - Mach
 - Mean = 0.2
 - Standard Dev = 0.02
 - Reynolds Number
 - 3.26 Million (MAC)/11,820 per inch
 - Standard Dev = 10%
- Epistemic - Interval
 - Angle of Attack – 8 & 16
 - ± 1.0 Degrees
- Latin Hypercube Sampling

P-Box 8 Deg – Medium Grid

$CL_{95}=1.782$



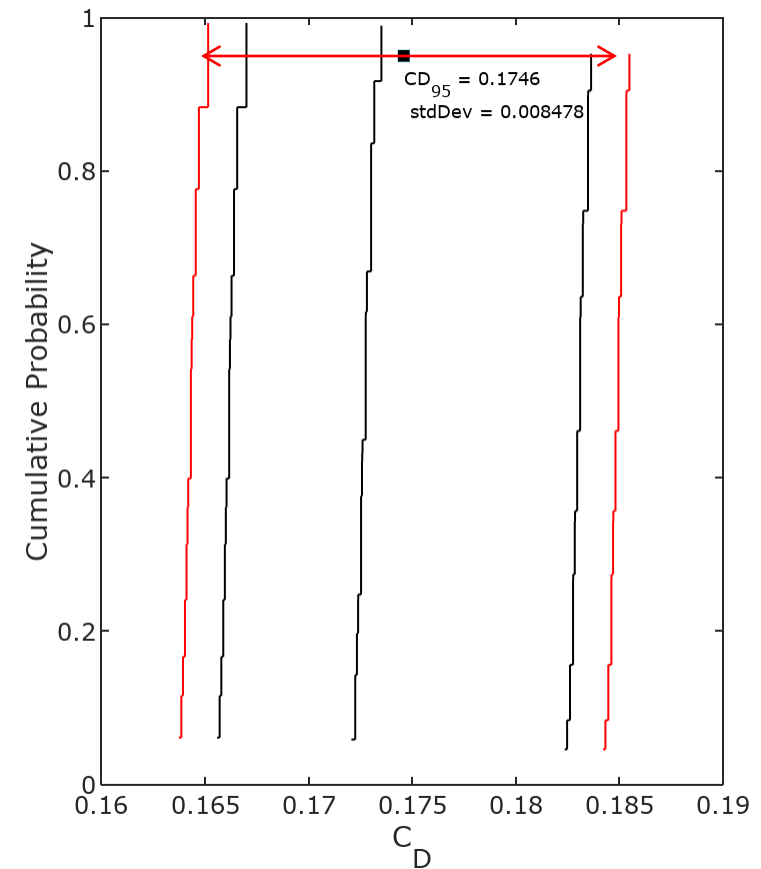
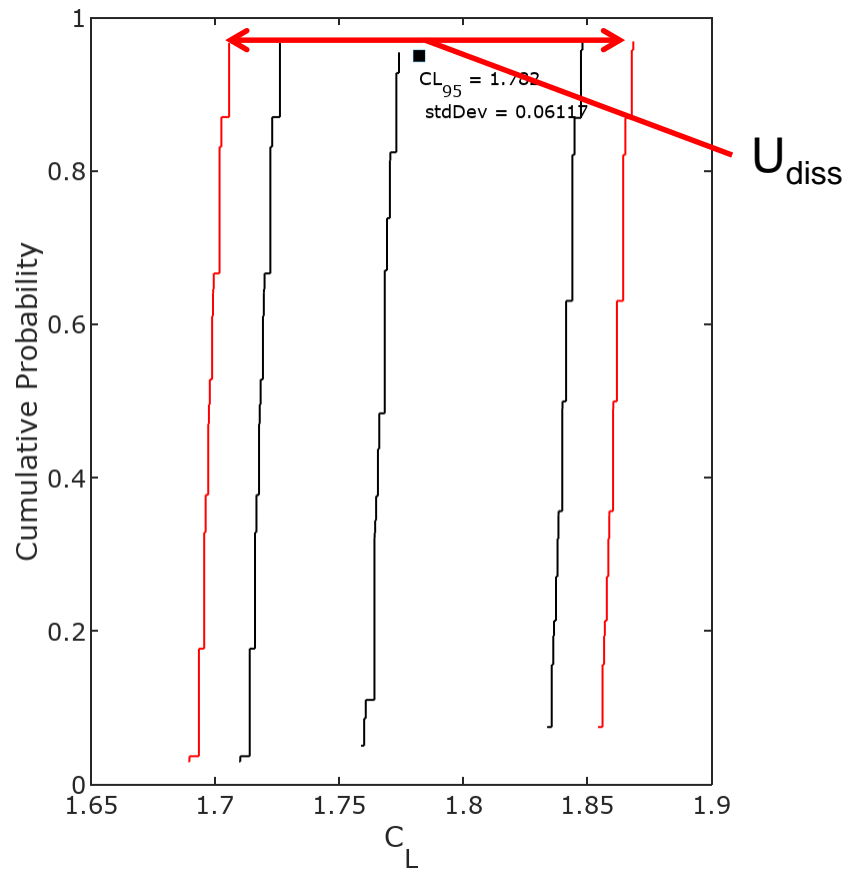
$CD_{95}=0.1746$



P-Box 8 Deg – Medium Grid

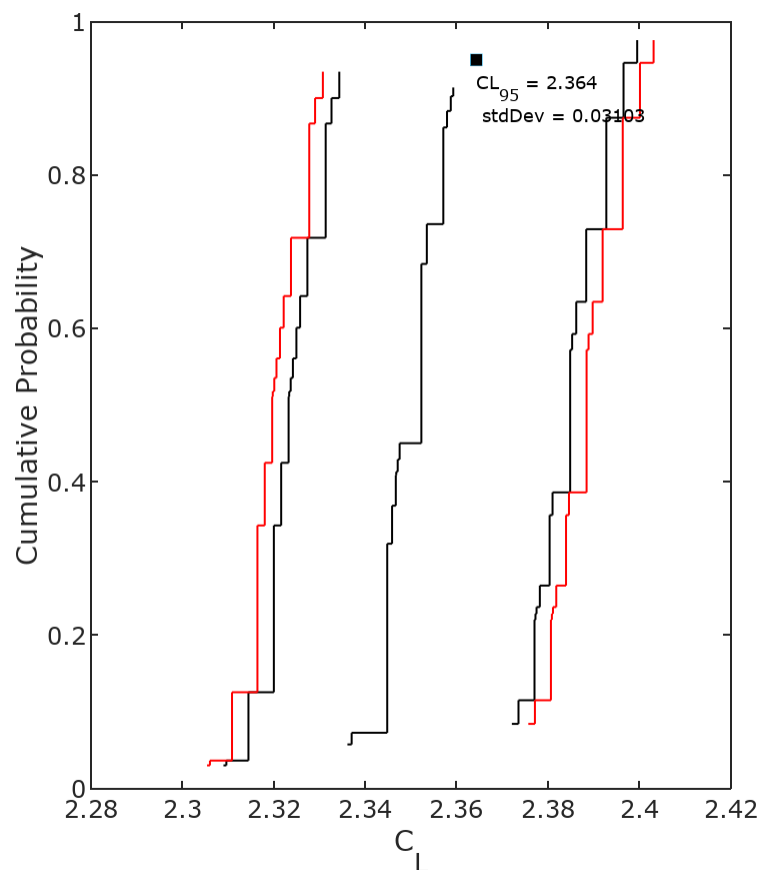
$CL_{95}=1.782$

$CD_{95}=0.1746$

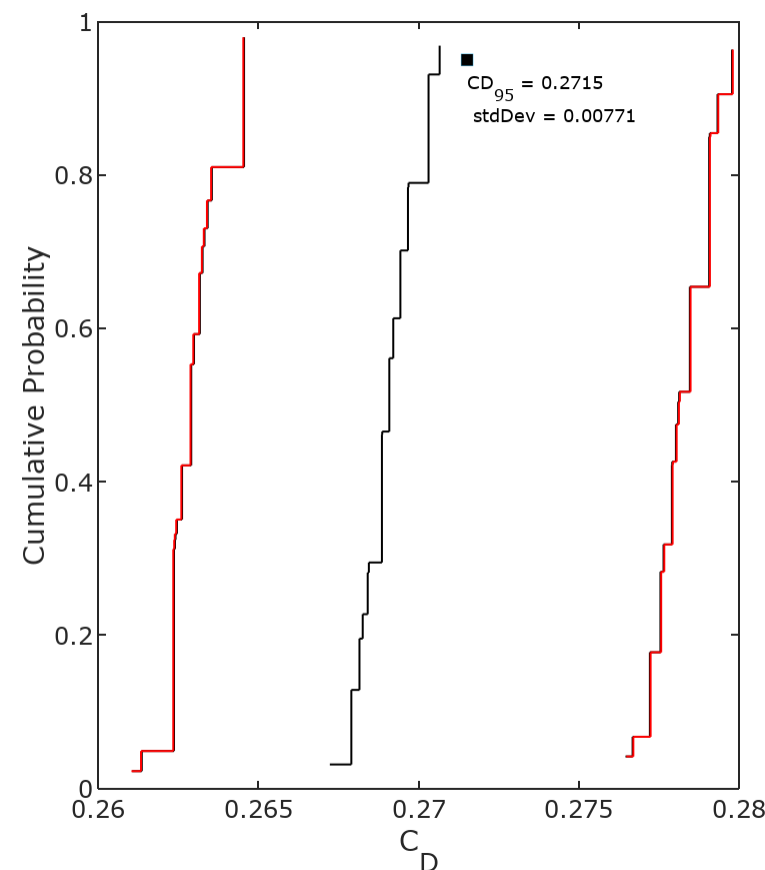


P-Box 16 Deg – Medium Grid

$CL_{95}=2.364$



$CD_{95}=0.2715$



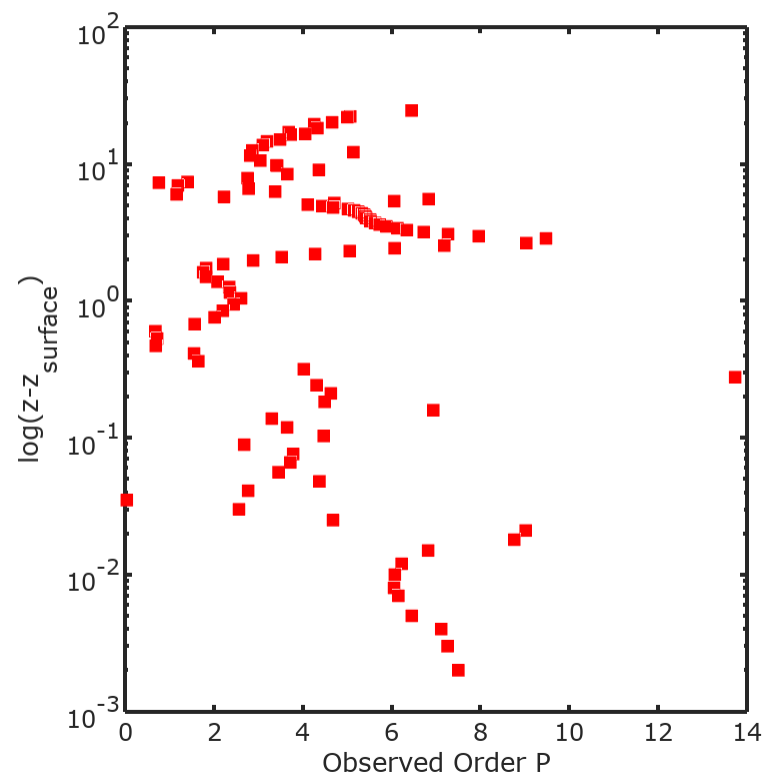
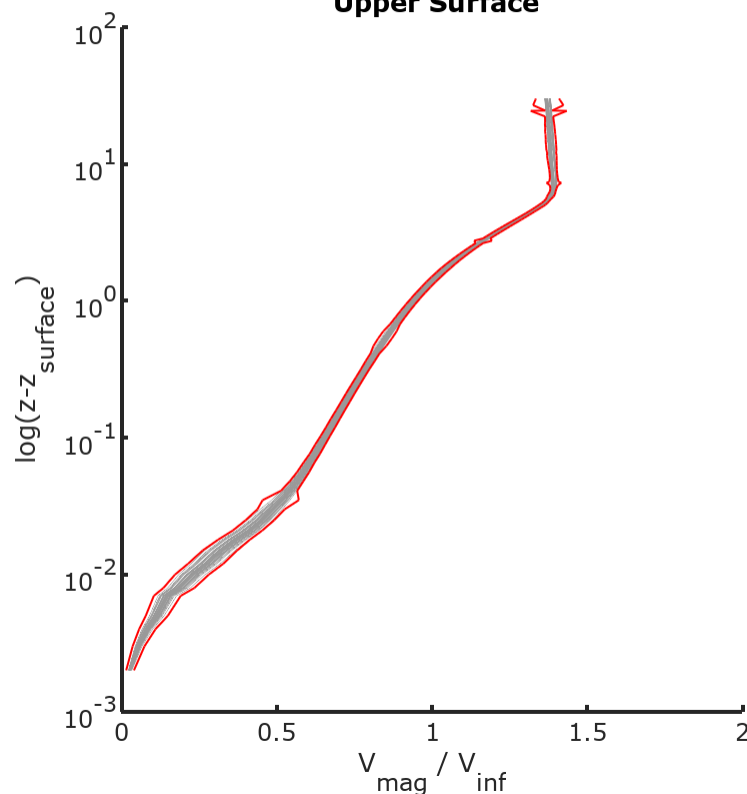
Velocity Plots – $\alpha_m = 8$

Velocity Magnitude Model Input Uncertainty

$\alpha_m = 8$

$x=1290.0, y=277.5$ Inches

Upper Surface



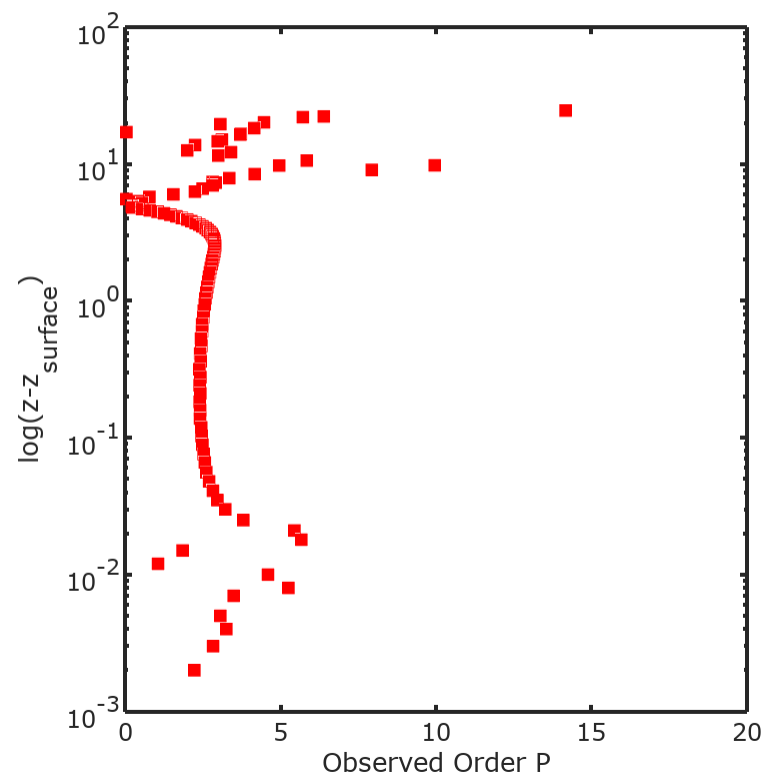
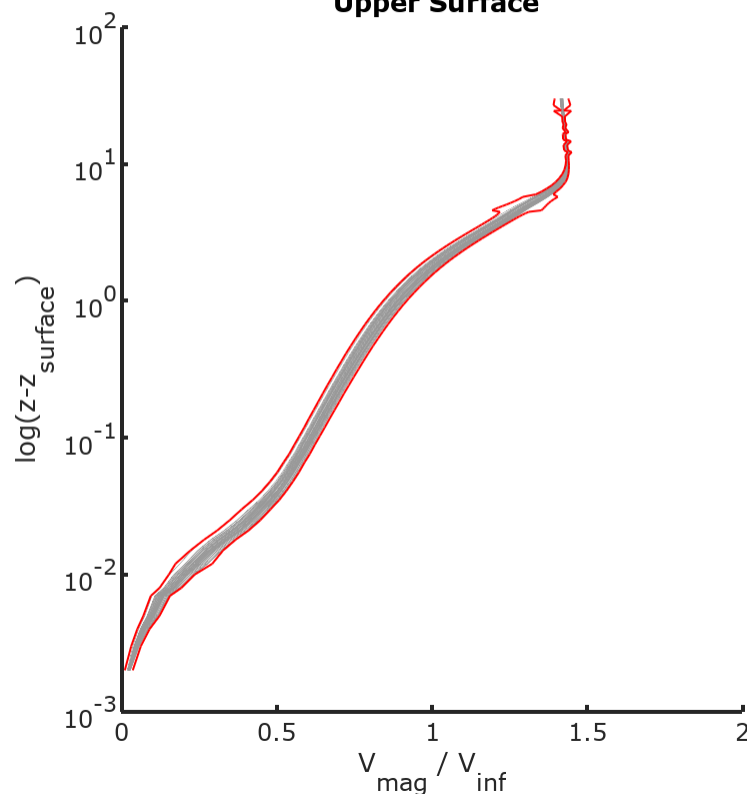
Velocity Plots – $\alpha_m = 16$

Velocity Magnitude Model Input Uncertainty

$\alpha_m = 16$

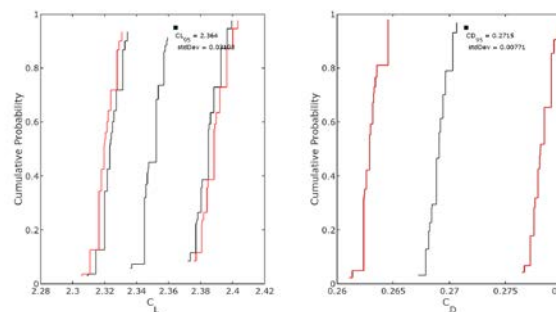
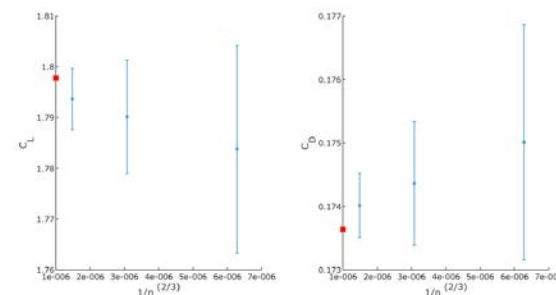
$x=1290.0, y=277.5$ Inches

Upper Surface

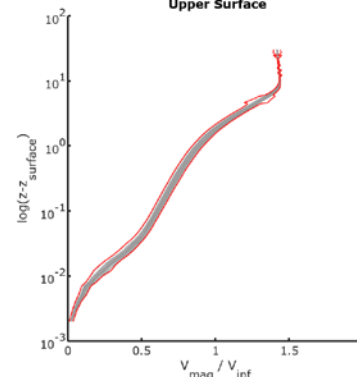


Summary

- UQ study of Case1a
 - U_{diss} & U_{model} Input
 - Global Uncertainty (CL,CD)
 - Local/Piecewise (Velocity Magnitude)
- Grid Convergence depends upon the flow condition
 - 8 deg converged monotonically
 - 16 deg oscillatory convergence
- Model Input
 - Mainly sensitive to angle of attack
 - 16 Deg more sensitive to Mach number than 8 deg
- Non-uniform refinement may be an issue for the UQ methods used
- Need to explore all the velocity profiles and C_p



Velocity Magnitude Model Input Uncertainty
 $\alpha_m = 16^\circ$
 $x=1290.0, y=277.5$ Inches
 Upper Surface



Acknowledgements

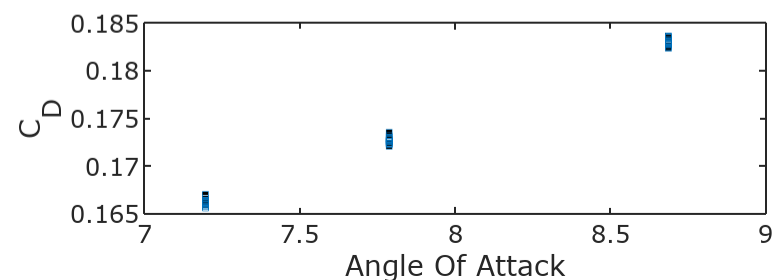
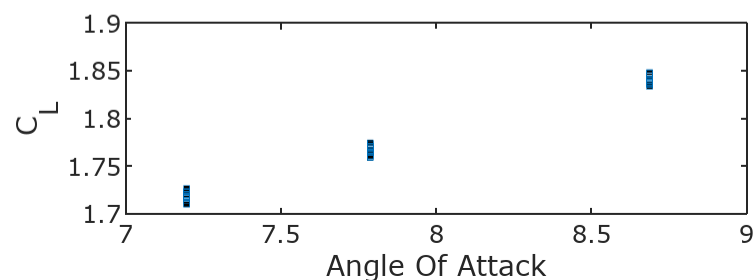
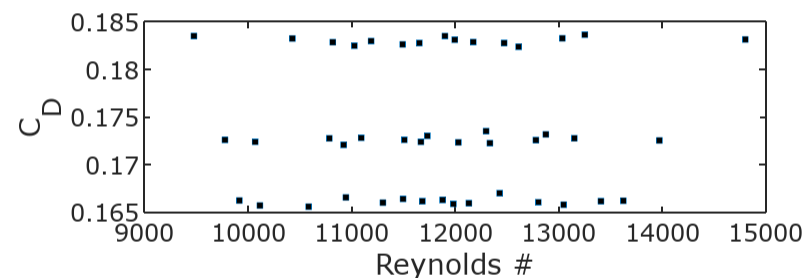
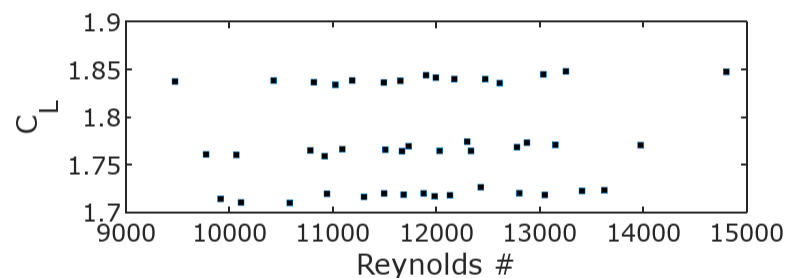
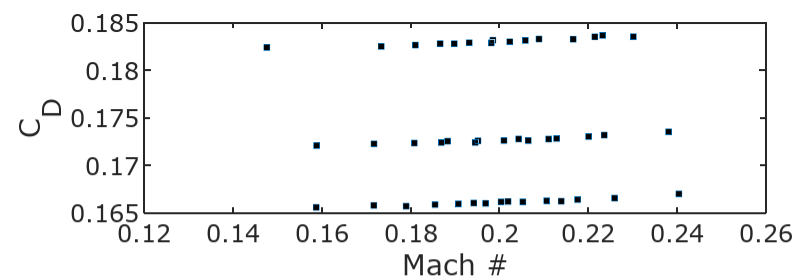
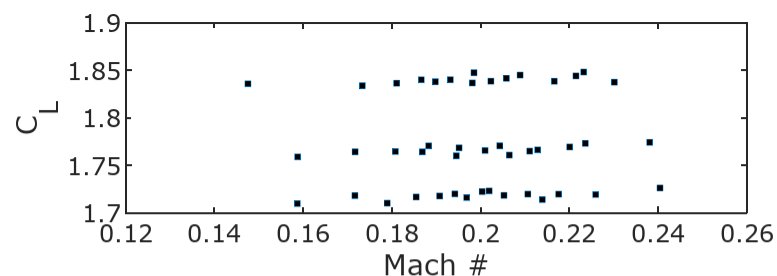
- The author would like to thank Cray Inc. for provided access to their corporate Cray XE40 computer
 - Geert Wenes and Greg Clifford of Cray Inc. for helping to acquire access.
 - David Whitaker from Cray Inc. for assistance in porting of OVERFLOW2 to the XE40 and for streamlining the use of FieldView on their system.
- This work could not have been accomplished without good overset grid systems. Thanks to the workshop team members for providing the grid and input files for OVERFLOW.
- Finally, much gratitude to Steve M. Legensky, General Manager and Founder at Intelligent Light, for his support of this work

References

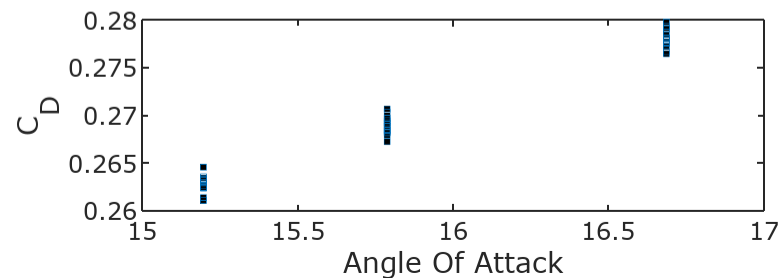
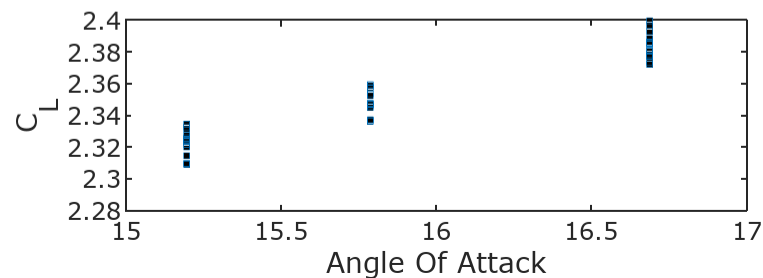
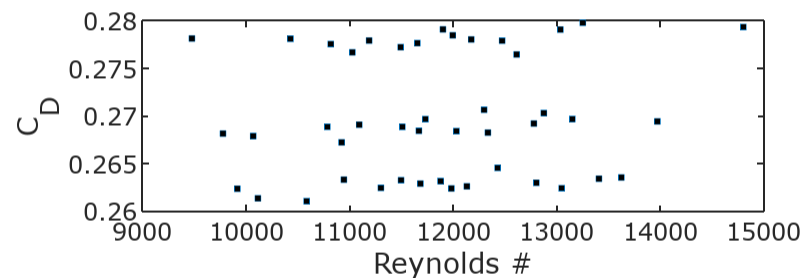
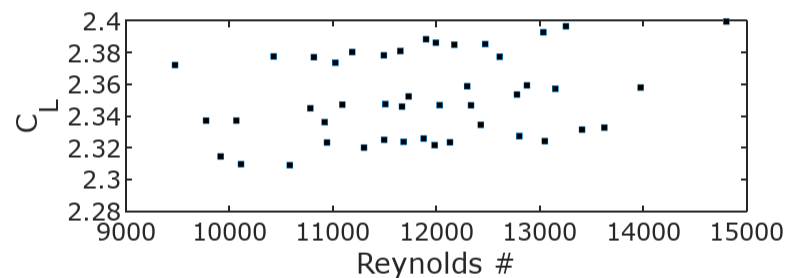
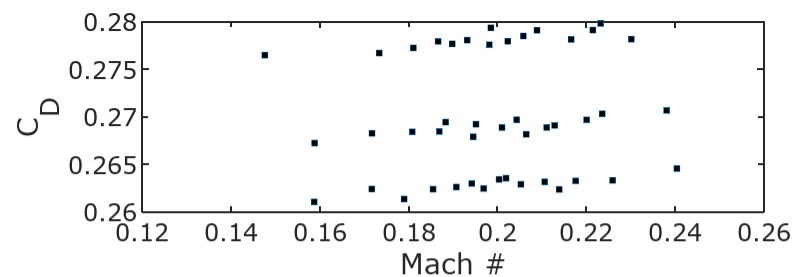
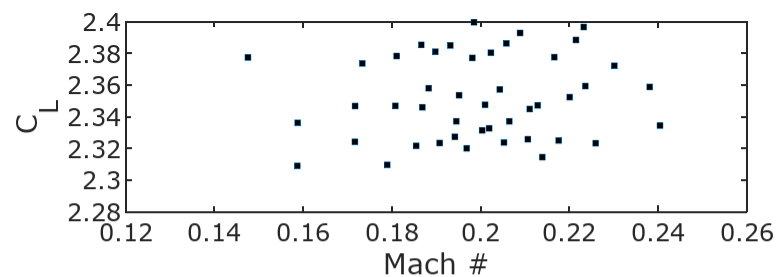
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- Standard for Verification and Validation in Computational Fluid Dynamics and Heat Transfer, ASME 2009, ISBN: 9780791832097
- William L. Oberkampf, Christopher J. Roy, *Verification and Validation in Scientific Computing*, Cambridge University Press, Oct 14, 2010

Additional Slides

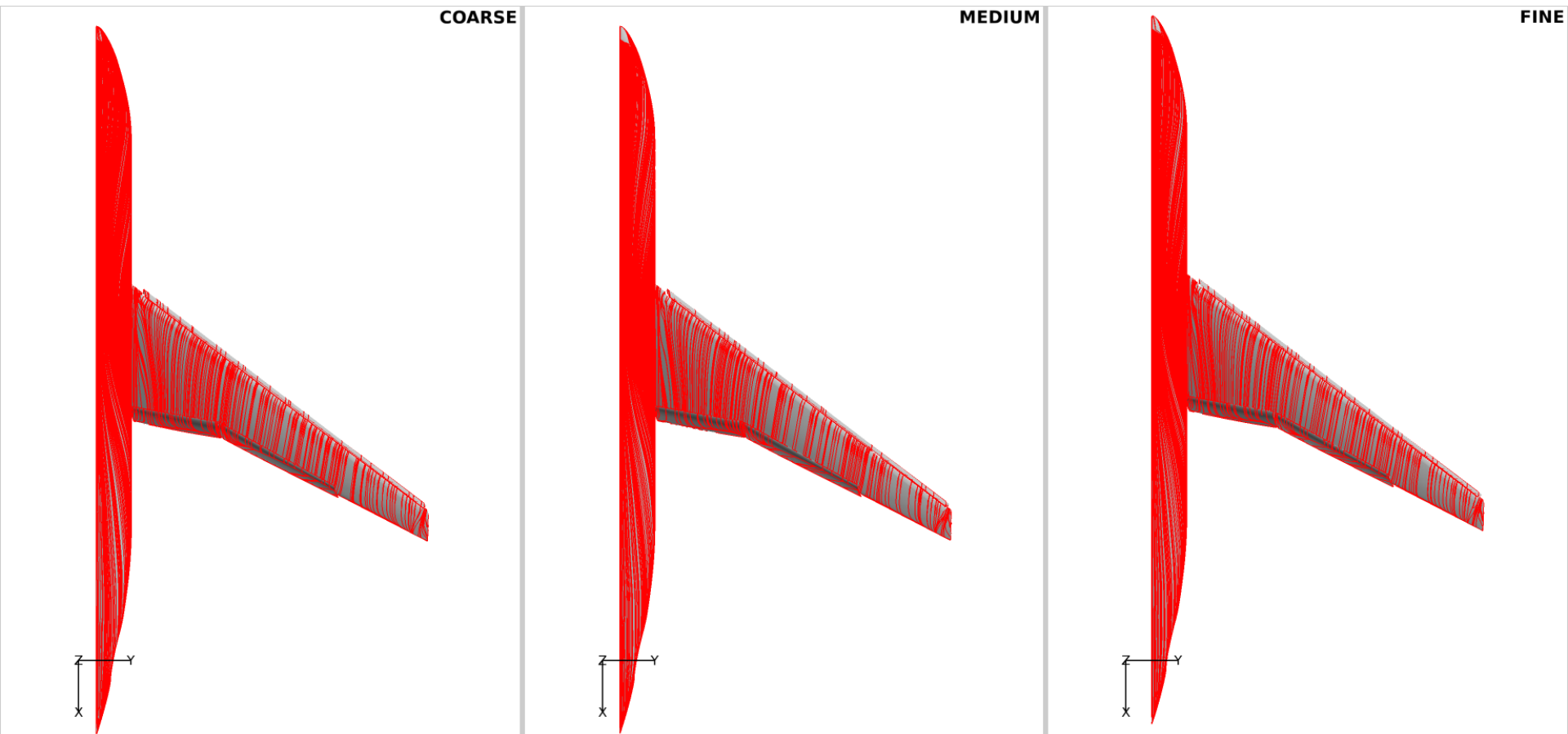
Sensitivity – 8 degs



Sensitivity – 16 degs

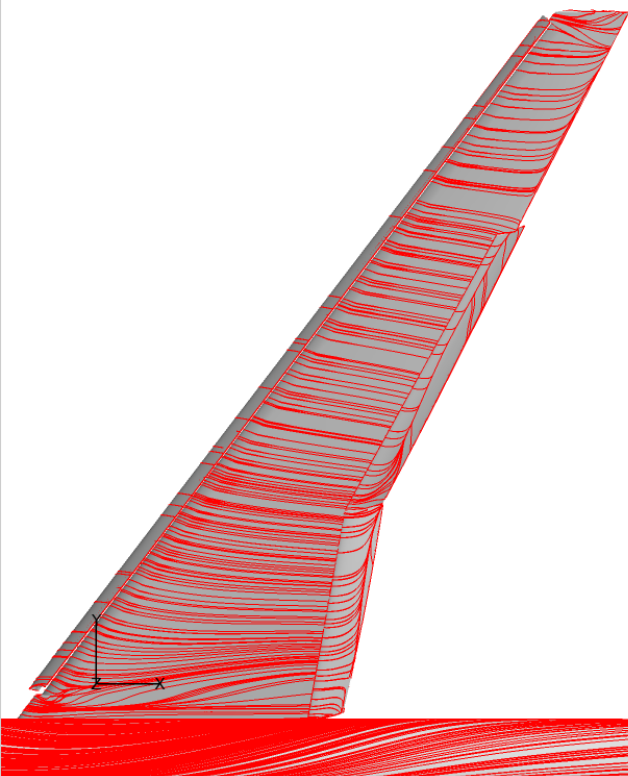


Visualizations

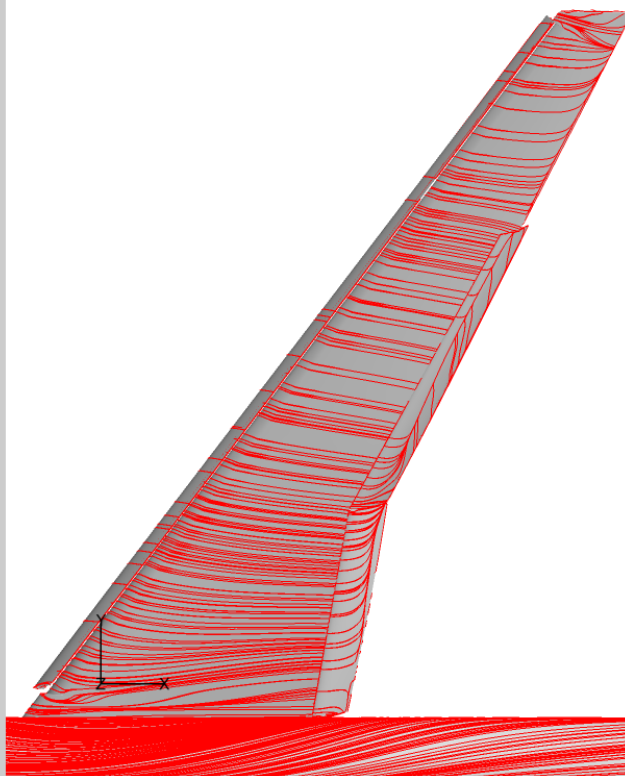




COARSE



MEDIUM



FINE

